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SOME FURTHER CONSIDERATIONS OF USING

FACTOR REGRESSION ANALYSIS

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Connett, Houston, and Shaw (1972) presented some advantages and uses of factor regression. I would like to suggest to anyone who is interested in this procedure a program developed by Finn (University of Chicago) who has done some work in this area.

Some Comment on Factor Regression

I. When using factor regression procedures, it is important to keep in mind that if one does not use all of the factors (that is, accounting for 100% of the trace) he may be overlooking a suppressor factor (suppressor variable). Whenever a set of predictor variables is factor analyzed, and accounts for 100% of the trace, and these factors are then used as the set of predictor variables in a multiple regression equation, then the two equations, the one based on the original variables and the other based on the factor variables, the two will make identical predictions (Darlington's Theorem #11 is proof of this statement.) It should be kept in mind, as Connett <u>et al</u>. (1972) pointed out, the factored multiple regression has advantages, such as orthogonality, which allows greater interpretation of the beta weights

¹Much of these comments are based on a paper by Darlington (1969).

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of the multiple regression equations.

II. If one is interested in improving the multiple regression equation by using factor techniques, there is only one way this can be done. That is if the number of factors that are used is less than the number of original variables. This will increase the df and also possibly decrease shrinkage-estimates. Because of this, some researchers have used only the few factors that account for the "greatest" amount of the factored trace. However, when this is done one may be losing information that can account for criterion variance by eliminating a factor that accounts for very little trace of the factored matrix but is highly correlated with the criterion scores.

III. An additional advantage of using factor scores is that when a matrix is factored much of the error variance tends to be distributed in the factors that account for the least variance. Therefore, one of the possible by-products of using factor scores which account for most trace variance as predictors is the likelihood of increasing reliability (therefore decreasing shrinkage).

Using only the factors that account for most of the trace should be avoided when the predictor variables that are being factored are likely to be highly reliable. Some examples of such variables are: height, weight, religion, sex, income, age, etc. Under these conditions a variable that accounts for little of the trace variance may be a good and highly reliable predictor of criterion variance.

IV. Connett <u>et al</u>. (1972) suggested that using factor regression should be of help when developing multiple regression equations for exploratory purposes. If one combines this factor regression procedure with stepwise procedures, some of the problems discussed in Sections I-III, can be considerably reduced. When stepwise procedures are employed, one

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should always use all the factors needed to account for 100% of the trace of the predictor variables.

As most of you are aware, the two basic stepwise procedures are stepup and stepdown. The advantages of each will not be discussed here but should be considered when one is choosing a stepwise procedure. 0ne concept of "tolerance" is not as widely familiar. "Tolerance" is a measure of how much a particular variable in an equation is a linear combination of the other variables in that equation. When there exists a perfect linear relationship, the "tolerance" will equal zero. If the "tolerance" of a particular variable is one, this means that the variable is adding an additional new dimension to the predictor equation which the other variables are not accounting for. The amount of additional variance accounted for by adding any variable is the product of the normalized regression coefficient squared and the "tolerance" of that variable. This "tolerance" procedure is used in the Stepwise Regression Program, in the Statistical Package for the Social Sciences (SPSS). When the factor regression procedure is used each factor will have, by definition, a "tolerance" equal to one. It can be seen how this "tolerance" procedure may allow one to use the original set of predictor variables and get much of the same information one would obtain by using factor regression procedure.

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PROOF THAT THE DEGREES OF FREEDOM FOR THE TRADITIONAL METHOD OF CALCULATING ANALYSIS OF COVARIANCE AND THE MULTIPLE REGRESSION METHOD ARE EXACTLY THE SAME

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Recently, a variety of publications (O'Conner, 1972; Kelly, Beggs, McNeil, 1969; Williams, Maresh, Peebles, 1972) have indicated that multiple regression is a very efficient method of calculating analysis of covariance. However, it is still unclear if the analysis of covariance, using the multiple regression approach suggested by Kelly, et al (1969), produces exactly the same result as the more traditional method of calculating analysis of covariance. The traditional method uses the residuals left after the variance of the criterion that can be accounted for by the covariate is subtracted. When comparing these two approaches, one may find differences due to incorrect calculations of the degrees of freedom (df) since it is easy to make an error in calculating the df when comparing the above two methods.

The following four models are presented to prove that the df's for both approaches are exactly the same:

Where: Y_1 = Posttest scores X_1 = 1 if the <u>S</u> is in Group 1: 0 otherwise

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 $\begin{array}{l} X_2 = 1 \mbox{ if the } \underline{S} \mbox{ is in the Control Group; 0 otherwise} \\ X_3 = \mbox{Pretest scores} \\ E_1 = Y_1 - \widehat{Y_1} \mbox{ (for Model 1)} \\ E_2 = \mbox{Residuals left after the variance that the pretest score accounts} \\ \mbox{ for is subtracted from the posttest score } (Y_1 - \widehat{Y_1} \mbox{ for Model 2}) \end{array}$

U = Unit vector; l if the <u>S</u> is in the sample; 0 otherwise a_0 , a_1 , a_2 , a_3 , = Partial regression weights

Let us also assume that N (the number of \underline{Ss}) = 100.

Model 1: $Y_1 = a_0U + a_1X_1 + a_2X_2 + a_3X_3 + E_1$ Restriction $a_1 = a_2$ Model 2: $Y_1 = a_0U + a_3X_3 + E_2$ Model 3: $E_2 = a_0U + a_1X_1 + a_2X_2 + E_3$ Restriction $a_1 = a_2$ Model 4: $E_2 = a_0U + E_4$

If one calculated the df needed for the F-ratio for testing Model 1 against

Model 2, the correct df would be:

df 1 = 3-2 = 1df 2 = 100-3 = 97

- where: df l = the number of linearly independent vectors in the full model (Model l) minus the number of linearly independent vectors in the restricted model (Model 2).
 - df 2 = the number of <u>independent</u> observations minus the number of linearly independent vectors in the full model.

If the df for testing Model 3 against Model 4 is calculated in exactly the

same way, one can easily make an error as follows:

df l = 1
df 2 =
$$100-2 = 98$$

This is an error. The following is a proof that the second set of df is incorrect since N is defined as the number of independent observations.

Theorum: In any sample of N observations, if multiple linear regression is performed on the model $Y_1 = E a_j X_{ij} + E_i$ given the least squares coefficients j=1 a_j , j = 1, 2, ..., n, then, given all values of the independent variables X_{ij} , and the coefficients a_j , and any N-m of the residuals E_i , the remaining m residuals can be computed.

Proof:

- (1) $E_i (Y_i a_j X_{ij}) = 0$ for any j
- (2) $Y_i = e_i + E_j a_j X_{ij}$ (model equation) substituting (2) into (1)
- (3) $E_i (a_i + E_j a_j X_{ij} a_j X_{ij}) = 0$ for any j each value of j gives a linear

equation in the missing e_i . Since j = 1, 2, ... n and there are m missing e_i , (3) gives m linear equations in m unknowns. Hence, the number of independent observations in the vector of residuals is N-m, not N.

The major point of this paper is that the df for both methods of calculating analysis of covariance are exactly the same. This does not mean that we believe the results will be exactly the same, for that is an emperical question (as Keith McNeil would say). To determine that, a Monte Carlo study is being planned. If you have any suggestions as to how we may best proceed, we would appreciate your comments.

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CONDITIONS FOR NO SECOND ORDER INTERACTION IN MULTIPLE LINEAR REGRESSION MODELS FOR THREE FACTOR ANALYSIS OF VARIANCE

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PART I - PICTORIAL OR GEOMETRIC APPROACH

Very little discussion is given on the subject of second order interaction in analysis of variance. Many texts, if they even discuss the matter, state the general mathematical condition (Kendall and Stuart (1) page 36)

$$\begin{array}{cccc} r & s & t \\ \Sigma & \Sigma & \Sigma & (\theta_{jkl})^2 = 0 \\ j=1 & k=1 & l=1 \end{array} \qquad \dots ... 1(a)$$

where

and dismiss the details as cumbersome or complex. Meyers (2) gives a set of conditions on the cell means, but does not explain that only a selected subset of the conditions are required and that the other conditions are redundant (duplicate the subset of conditions). Winer (3) endeavours to give a pictorial explanation of no second order interaction which on closer examination is found to deal with only one very special case. This will be discussed in section 1 where a three factor 2*2*2 design is considered. In section 2 the results of section 1 will be generalized to cases where more than two levels occur in a factor. To avoid complicating the description, the following assumption will be added to the normal statistical requirements:

1) The number of scores per cell is the same for each cell,

namely, n.

2) The scores are not subject to numerical error.

The difficulties and complications that can arise in two factor designs if assumption 1) is violated have been discussed by White (4). A good text on industrial statistics should discuss the effect of assumption 2).

1. In this section we will discuss the condition for no second order interaction in a three factor 2*2*2 design. Firstly, we will formally state the two multiple linear regression models required, and will subsequently give a primarily pictorial (geometric) explanation of the restriction required for model 2. The three factors will be labelled A, B and C, and individual cells will be referred to by factors and levels. For example, AlB2C2 will refer to the cell at level 1 of factor A, level 2 of factor B and level 2 of factor C.

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Model 1 No restriction

$$y = a_1 \underline{x}_1 + a_2 \underline{x}_2 + a_3 \underline{x}_3 + a_4 \underline{x}_4 + a_5 \underline{x}_5 + a_6 \underline{x}_6 + a_7 \underline{x}_7 + a_8 \underline{x}_8 + \underline{e}_1 \quad \dots 2(a)$$

Model 2 Restriction for no second order interaction

$$(a_{4} - a_{3}) - (a_{2} - a_{1}) = (a_{8} - a_{7}) - (a_{6} - a_{5}) = I \qquad \dots 2(b)$$

$$y = a_{1}\underline{x}_{1} + a_{2}\underline{x}_{2} + a_{3}\underline{x}_{3} + (I + a_{3} + (a_{2} - a_{1})) \underline{x}_{4}$$

$$+ a_{5}\underline{x}_{5} + a_{6}\underline{x}_{6} + a_{7}\underline{x}_{7} + (I + a_{7} + (a_{6} - a_{5}))\underline{x}_{8} + \underline{e}_{1}$$

or $y = a_{1}(\underline{x}_{1} - \underline{x}_{4}) + a_{2}(\underline{x}_{2} + \underline{x}_{4}) + a_{3}(\underline{x}_{3} + \underline{x}_{4}) + I(\underline{x}_{4} + \underline{x}_{8})$

$$a_{5}(\underline{x}_{5} - \underline{x}_{8}) + a_{6}(\underline{x}_{6} + \underline{x}_{8}) + a_{7}(\underline{x}_{5} + \underline{x}_{8}) + \underline{e}_{1} \qquad \dots 2(c)$$

where the subscript 1 refers to the cell AlBlC1,

88	66	2	88	\$8 88	8 8	A2B1C1,
	88	3	49 69	88 88	6 8	AlB2C1,
8 8	51	l3	£8	((88	A2B2C1,
500 e	86	5	51	21 4 8		A1B1C2,
\$9	61	6	55	88 S S	88	A2B1C2,
59	8 8	7	85	16 1 6	85	AlB2C2,
6 8	8 n	8	0 2	55 55	8 5	A2B2C2.

The column vectors \underline{y} and \underline{x}_i , i = 1, 2, ..., 7, 8 are of length $2_{\pm}2_{\pm}2_{\pm}n$ Scores from all cells are arranged systematically in the vector \underline{y} . The vectors \underline{x}_i are defined as follows:

an element of the vector $\underline{x}_i = \begin{cases} 1 & \text{if the corresponding element} \\ & \text{of } \underline{y} \text{ is a score from the cell } i. \end{cases}$ 0 otherwise.

The parameters a_i and I are determined by a least squares fit which minimizes $\underline{e_1}^T \underline{e_1}$ in model 1 and $\underline{e_I}^T \underline{e_I}$ in model 2, where \underline{e}^T denotes the transpose of the column vector \underline{e} (that is a row vector with the same elements as \underline{e}). For the reader not familiar with matrix notation the quantity $\underline{e_1}^T \underline{e_1}$ is just the error sum of squares for model 1. Note the value of a_i computed by model 1 will be the mean of the scores from cell i.

To test for a significant second order interaction the following F statistic with (r-1)(s-1)(t-1) and (rst(n-1)) degrees of freedom is computed

$$F = \frac{(ESS_1 - ESS_1)/(r-1)(s-1)(t-1)}{(ESS_1)/(rst(n-1))} \dots 2(d)$$

where $ESS_1 = \underline{e_1} \underline{e_1}$,

 $ESS_I = e_I^T e_I$,

 r_ss_s and t are the number of levels for factors A,B and C respectively (in this case r=s=t=2), and n is the number of observations per cell.

To simplify the later discussion a measure of first order interaction for a 2*2 design will be given. For this purpose consider the Cl level in the 2*2*2 design under discussion. This involves the cells with





Fig. 1(b)

index i = 1, 2, 3, 4. A measure I_{1234} of the first order interaction over the

face 1234 of the cube given in figures 1(a) and 1(b) is defined by the equation

$$I_{1234} = (a_{1} - a_{3}) - (a_{2} - a_{1}) .$$

It should be noted at this point that the orientation of the corner points of the face must be consistently ordered when evaluating the right hand side of the equation. For example:

$$(a_3 - a_4) - (a_1 - a_2) = - I_{1234}$$

does not equal I _____ Similarly

 $(a_2 - a_1) - (a_4 - a_3) = I_{3412} \neq I_{1234}$

We can now state the restriction or condition for no second order interaction in a 2*2*2 design as follows:

$$I_{1234} = I_{5678} = I_{...3(a)}$$

or
$$(a_4 - a_3) - (a_2 - a_1) = (a_8 - a_7) - (a_6 - a_5) = 1 \dots 3(b)$$

This restriction states that the first order interaction over the face 1234 equals the first order interaction over the perpendicularly opposite face 5678 or the first order interaction is constant over the perpendicularly opposite C1 and C2 faces.

The faces in a 2*2*2 design are just "squares", but if more levels in a factor are considered a face consists of several "squares" (see figures 4(a) and 4(b)). For convenience in section 2 we will refer to these "squares" as panels. For example, in 4*3*3 design the Cl face would contain (4-1)*(3-1)= 6 panels (see figure 5). Returning to our simple 2*2*2 design, we could obtain two further restrictions by equating first order interactions over

(1) the Al and A2 faces or the panels 1537 and 2648

and (ii) the B1 and B2 faces or the panels 1256 and 3478 This gives the equations

> $(a_7 - a_3) - (a_5 - a_1) = (a_8 - a_4) - (a_6 - a_2) = I_A \dots 4(a)$ $(a_6 - a_5) - (a_2 - a_1) = (a_8 - a_2) = (a_4 - a_3) = I_B \dots 4(b)$

and

For uniformity of notation we could replace I in equation 3(b) by $I_{\underline{C}}$ as the equation relates to interactions over the Cl and C2 faces.

$$(a_4 - a_3) - (a_2 - a_3) = (a_8 - a_7) - (a_6 - a_5) = I_C \dots 4(c)$$

Though I_A , I_B and I_C are not equal the relations between the parameters a_i in 4(a), (b) and (c) are equivalent. For example, consider 4(a)

$$(a_7 - a_3) - (a_5 - a_1) = (a_8 - a_4) - (a_6 - a_2)$$

Add $(a_4 - a_2 - a_7 + a_5)$ to each side. The terms in a_7 and a_5 cancel on the left and the terms in a_4 and a_2 cancel on the right of the equation giving the equation

or
$$(a_{4} - a_{3}) - (a_{2} - a_{1}) = (a_{6} - a_{7}) - (a_{6} - a_{5})$$

which is exactly the relation between the parameters a_i given by equation 4(c) It can be similarly shown that relation 4(b) is equivalent to the relations 4(a) and 4(c). Hence it is only necessary, and in fact sufficient, to use one of the three relations obtained by considering the faces of the cube given in figures 1(a) and (b). That the relations given above do guarantee no second order interaction will be proved mathematically in part II of this paper.

We now consider the pictorial explanation given in Winer (3) on pages 182 to 184.

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Winer (3) gives an example like example 1 below.

, , ,		01		· · ·	c 2	
	Surpresentation	B 1	В2	ه ۰ ۰	B .	в 2
A	1	2	8	A 1	4	10
A	2	2	4	A 2	4	6
Ölminin andrayaşını analaşını analaşını analaşını analaşını analaşını analaşını analaşını analaşını analaşını a						

Table 1 - Cell Means for example 1

The means for this example are shown diagramatically in figures 2(a) and (b).



Note the shaded areas in figures 2(a) and 2(b) are similar. This similarity of shape, Winer gives as a condition for no second order interaction. Certainly the cell means for example 1 satisfy the condition 4(c)

(4 - 8) - (2 - 2) = (6 - 10) - (4 - 4)

Now consider the following set of data.



Table 2 - Cell Means for example 2

We illustrate the means for example 2 diagramatically in figures 3(a) and (b).



No similar shapes can be observed in figures 3(a) and (b), but the data does satisfy the restriction 4(c).

(5-4) - (2-6) = (9-6) - (2-4)

There is no second order interaction for the data of example 2, even though "Winer's condition" is violated. The "Winer condition" is a special case of the completely general condition given in this paper. 2. How do these ideas generalize in the case of more than two levels for each factor? There are now many "cubes" of the type shown in figures 1(a) and (b). This is illustrated by figures 4(a) and (b), and figure 5. For simplicity we now consider a 3*2*2 design shown diagramatically in figures 4(a) and (b).

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The rectangular block in figures 4(a) and (b) is split into two 2*2*2 cubes by level 2 of A. It was noted in section 1 that a cube produces 3 restrictions, 2 of which are redundant. The two cubes will produce 6 restrictions, 4 of which are redundant. There are three alternative ways of selecting 2 non-redundant restrictions as follows:

(i) Equate the BC first order interactions on the facesA1, A2 and A3. That is

$$I_{1,7,4,10} = I_{2,8,5,11} = I_{3,9,6,12} = I_A$$
5(a)

(ii) Equate the AC first order interactions for the two panels on the B1 and B2 faces. That is

$$I_{1,2,7;8} = I_{4,5,10,11} = I_{B_1}$$
, ...5(b)

and

 $I_{2,3,8,9} = I_{5,6,11,12} = I_{B_2}$

•••5(c

panels on the Cl and C2 faces. That is

$$I_{1,2,4,5} = I_{7,8,10,11} = I_{C_1}$$
,5(d)

and

$$I_{2,3,5,6} = I_{8,9,11,12} = I_{C_2}$$
5(c)

Any one of the pairs (i), (ii) or (iii) are necessary, and in fact sufficient, conditions for no second order interaction in a 3*2*2 design. It can be noted here that "Winer's condition" is sufficient, but not necessary.





A general rule emerges. Take all panels on the face Al. Then equate the first order interaction on each of these panels with the interaction on the corresponding panels at every other level of Λ . If we are considering a r*s*t design there are (s-1)(t-1) panels on the Al face. Each of these panels will produce (r-1) restrictions. Hence there is a total of (r-1)(s-1)(t-1) restrictions. For the case of 4*3*3 design there are (4-1)(3-1)(3-1)=16 restrictions. We could equally well have taken the (r-1)(t-1) panels on the B1 face and equate interactions on the corresponding panels at the (s-1) other levels of factor B. Again (r-1)(s-1)(t-1) restrictions are generated. This is exactly the number of cubes in the design. For each cube there is one restriction from the set generated by Al and one restriction from the set of restrictions generated by B1. But the restriction given by two A faces of a cube and the restriction given by two B faces are equivalent. Hence the first set of restrictions is duplicated by ,the second set of restrictions. A third set of restrictions based on Cl and other levels of C will again duplicate the first set of restrictions and consequently duplicate the second set of restrictions. Let us finally give the 'models for a 3*2*2 design.

Model 1 No restriction

$$\underline{y} = a_{1}\underline{x}_{1} + a_{2}\underline{x}_{2} + a_{3}\underline{x}_{3} + a_{4}\underline{x}_{4} + a_{5}\underline{x}_{5} + a_{6}\underline{x}_{6}$$

+ $a_{7}\underline{x}_{7} + a_{8}\underline{x}_{8} + a_{9}\underline{x}_{9} + a_{10}\underline{x}_{10} + a_{11}\underline{x}_{11} + a_{12}\underline{x}_{12} + \underline{e}_{1}$...6(a)

Model 2

Restriction for no second order intersection

$$(a_{10} - a_4) - (a_7 - a_1) = (a_{11} - a_5) - (a_8 - a_2) = \dots 6(b)$$

= $(a_{12} - a_6) - (a_9 - a_3) = I_A$
$$\underbrace{y}_{i=1}^{9} a_i \underbrace{x}_{i=i} + \{I_A + a_4 + (a_7 - a_1)\} \underbrace{x}_{10}$$

+ $\{I_A + a_5 + (a_8 - a_2)\} \underbrace{x}_{11}$
+ $\{I_A + a_6 + (a_0 - a_2)\} \underbrace{x}_{12} + e_7$

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or
$$\underline{y} = a_1(\underline{x}_1 - \underline{x}_{10}) + a_2(\underline{x}_2 - \underline{x}_{11}) + a_3(\underline{x}_3 - \underline{x}_{12})$$

+ $a_4(\underline{x}_4 + \underline{x}_{10}) + a_5(\underline{x}_5 + \underline{x}_{11}) + a_6(\underline{x}_6 + \underline{x}_{12})$
+ $a_7(\underline{x}_7 + \underline{x}_{10}) + a_3(\underline{x}_8 + \underline{x}_{11}) + a_9(\underline{x}_9 + \underline{x}_{12})$
+ $I_A(\underline{x}_{10} + \underline{x}_{11} + \underline{x}_{12}) + \underline{e}_I$

where the indexing is consistent with figures 4(a) and (b), and the definition of the vectors \underline{x}_i and \underline{y} is essentially the same as for equations 2(a) and (c). Note the parameters a_i computed by least squares for Model 1, will not in general be equal to the parameters a_i computed for Model 2.

...6(c)

A final word of warning is that second and higher order interactions must be interpreted with great care, if meaningless or erroneous conclusions are not to be drawn from research data.

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A Note on the Independent Variance of Each Criterion in a Set

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Frequently a researcher is interested in a number of criterion variables which may not be uncorrelated with each other. An example of such criterion variables may be History GPA Y_1 , Math GPA Y_2 , and Reading GPA Y_3 . The chances are that these variables are likely to be significantly correlated with each other.

If one developed a regression equation trying to predict Y_p , (History GPA) from socioeconomic status (X_1) it would be presented in the form of Model 1.

Model 1 $Y_1 = a_0 U + a_1 X_1 + E_1$

One can test to see how much of the criterion variance is accounted for by looking at the R^2 . However, if the researcher is interested in determining how much of the criterion variance X_1 can account for of Y_1 , that is independent of Y_2 and Y_3 , he can test Model 2 against Model 3.

Model 2 $Y_1 = a_0 U + a_1 X_1 + a_2 Y_2 + a_3 Y_3 + E_2$ Model 3 $Y_1 = a_0 U + a_1 Y_2 + a_2 Y_3 + E_3$

By testing Model 2 against Model 3 we are testing the amount of variance of Y_1 that is independent of Y_2 and Y_3 , that can be accounted for by X_1 .

If we follow this exact procedure for predicting Y_2 and Y_3 , the three F tests that would be run, for Y_1 , Y_2 and Y_3 , would be independent of each other. Therefore the probability of making a Type I error for each test would be equal to \mathcal{L} (assuming the underlying assumptions of normality and homogeneity of variance are met). Another way of looking at this is if one did not covary the additional criterion variables, one would be required to use some multiple comparison correction since the three F ratios for the three criterion variables would not be independent of each other. For example, if we use the concept $\frac{e^{-1}}{N}$ (where N = number of nonindependent F-tests calculated and \mathcal{K} = the desired level we want to hold constant) for this purpose then the N, for the first case, where the criterion variables were covaried would be equal to one since all three F ratios would be independent of each other. However, in the second case where the criterion variables are not covaried, the F ratios would not be independent and, therefore, N would be equal to three.

If there is more than one predictor variable, X_1 (Socioeconomic status), X_2 (Sex), X_3 (Years in school) and X_4 (Age), and we were interested in determining how much of the independent variance of the criterion each of these variables accounted for, one would test Model 4 against Model 5, Model 4 against 6, Model 4 against 7, and Model 4 against 8. A similar procedure would be followed for criterion variables 2 and 3. The N then needed for $\frac{\mathcal{L}}{N}$ multiple comparison correction would then be 12 (four for testing Y_1 , four for Y_2 and four for testing Y_3 since Y_1 , Y_2 and Y_3 are not independent of each other.

Model 4 $Y_1 = a_0U + a_1X_1 + a_2X_2 + a_3X_3 + a_4X_4 + E_4$ Model 5 $Y_1 = a_0U + a_2X_2 + a_3X_3 + a_4X_4 + E_5$ Model 6 $Y_1 = a_0U + a_1X_1 + a_3X_3 + a_4X_4 + E_6$ Model 7 $Y_1 = a_0U + a_3X_1 + a_2X_2 + a_4X_4 + E_7$ Model 8 $Y_1 = a_0U + a_1X_1 + a_2X_2 + a_3X_3 + E_8$

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¹This formula and proof has been presented in <u>Multiple Linear Regression</u> Viewpoints Vol. 2, No. 3, Jan. 1972, by Newman & Fry, p. 36-39.

However, if models similar to Models 9 and 10 which covaried the additional criterion variables were used following the same procedure that was in the above test for each of the criterion variables: Y_1 , Y_2 and Y_3 , the N needed for the $\frac{c}{N}$ multiple correction, would be 4 instead of 12.

Model 9 $Y_1 = a_0U + a_1X_1 + a_2X_2 + a_3X_3 + a_4X_4 + a_5Y_2 + a_6Y_3 + E_9$ Model 10 $Y_1 = a_0U + a_2X_2 + a_3X_3 + a_4X_4 + a_5Y_2 + a_6Y_3 + E_{10}$

As suggested above, by covaring other nonindependent criteria that we are interested in, we can actually treat each test of each criterion as if the criterion variables were independent of each other. Of course, testing Model 9 versus 10 answers a different question than does testing Model 4 versus 5. The question one wants to ask should always dictate the models used. What we are saying here is that if one is interested in accounting for the independent piece of a criterion variable's variance, then the procedures outlined here should be used.

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